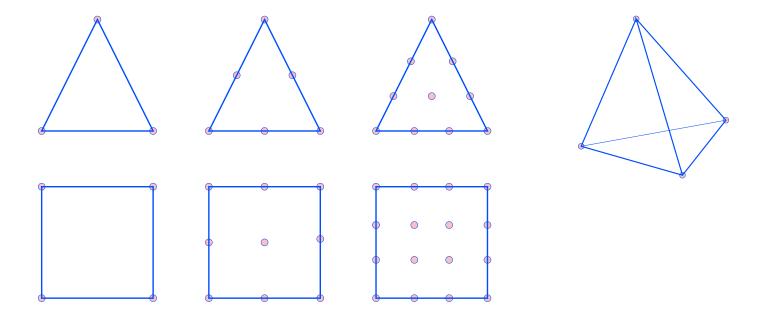
# CCM, Part III (3)

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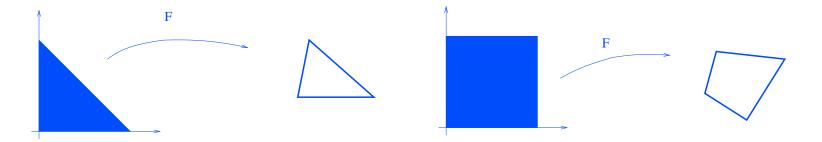
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#### Generalization to more space dimensions

Example of unisolvent degrees of freedom



How to construct stiffness matrix and load vector In general one considers reference elements and mappings to actual elements



Notation:  $\hat{K}$  reference element; K actual element  $\hat{\varphi}_1, \dots \hat{\varphi}_N$  reference shape functions;  $\varphi_1, \dots \varphi_N$  actual shape functions

How to map the shape functions

$$F_K : \hat{K} \to K, \quad \vec{x} = F(\hat{\vec{x}})$$
  
$$\varphi(\vec{x}) = \hat{\varphi}(F^{-1}(\vec{x}))$$

Example of computation of *local* stiffness matrix (one dimensional)

$$A_{ji} = a(\varphi_i, \varphi_j) = \int_a^b \varphi_i'(x)\varphi_j'(x) dx = \sum_K \int_K \varphi_i'(x)\varphi_j'(x) dx$$
$$\int_K \varphi_i'(x)\varphi_j'(x) dx = \int_{\hat{K}} \frac{\hat{\varphi}_i'(\hat{x})}{F'(\hat{x})} \frac{\hat{\varphi}_j'(\hat{x})}{F'(\hat{x})} F'(\hat{x}) d\hat{x} = \int_{\hat{K}} \frac{\hat{\varphi}_i'(\hat{x})\hat{\varphi}_j'(\hat{x})}{F'(\hat{x})} d\hat{x}$$

$$\int_{\hat{K}} \frac{\hat{\varphi}_i'(\hat{x})\hat{\varphi}_j'(\hat{x})}{F'(\hat{x})} \, d\hat{x}$$

In general,  $F = \alpha + \beta \hat{x}$  is affine so that  $F' = \beta$  is constant (and equal to h)

$$\int_{\hat{K}} \frac{\hat{\varphi}_i'(\hat{x})\hat{\varphi}_j'(\hat{x})}{F'(\hat{\vec{x}})} dx = \frac{1}{h} \int_{\hat{K}} \hat{\varphi}_i'(\hat{x})\hat{\varphi}_j'(\hat{x}) dx$$

In more space dimensions, F is affine for more popular elements.

$$\int_{K} \vec{\operatorname{grad}} \, \varphi_{i}(\vec{x}) \cdot \vec{\operatorname{grad}} \, \varphi_{j}(\vec{x}) \, d\vec{x} = ?$$

General strategy for assembling the stiffness matrix and the load vector

- ▶ Loop over elements ie = 1, ..., ne
- Compute local stiffness matrix  $A_{ji}^{loc}=a(\varphi_i,\varphi_j)$ ,  $i,j=1,\ldots,ndof$  and local load vector  $F_i^{loc}=F(\varphi_i)$ ,  $i=1,\ldots,ndof$
- ▶ Loop for i, j = 1, ..., ndof and assembly of global matrix

$$A_{iglob,jglob} = A_{iglob,jglob} + A_{ij}^{loc}$$

Account for boundary conditions

Some remarks on the discrete linear system

- matrix is sparse (sparsity pattern, so called skyline, can be determined a priori
- matrix is SPD (CG can be succesfully applied)
- ightharpoonup conditioning of matrix grows as h goes to zero (need for preconditioning)

#### **Convection diffusion equation**

As usual. . . a one dimensional example

$$\begin{cases} -\varepsilon u''(x) + bu'(x) = 0 & 0 < x < 1 \\ u(0) = 0, \ u(1) = 1 \end{cases}$$

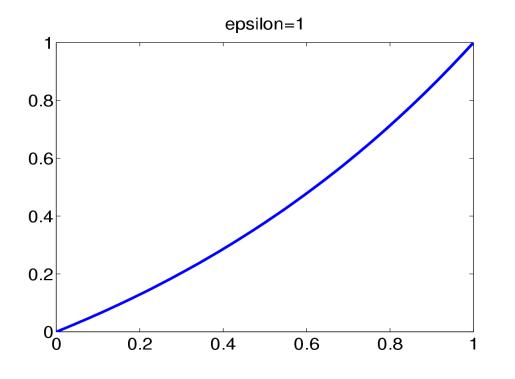
Non-homogeneous boundary conditions (!) Péclet number  $\mathbb{P} = |b|L/(2\varepsilon)$  (L=1 in our case)

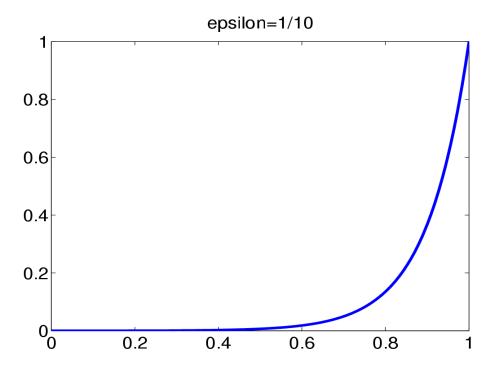
Closed form solution can be explicitly computed

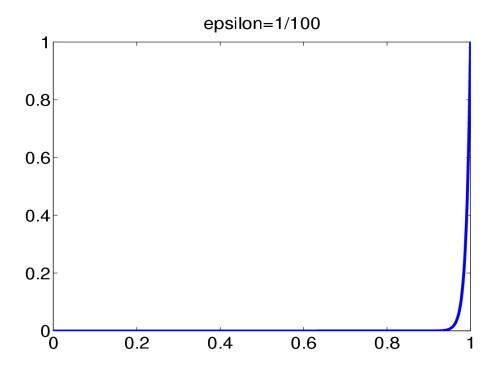
$$u(x) = \frac{\exp(bx/\varepsilon) - 1}{\exp(b/\varepsilon) - 1}$$

### Convection diffusion equation (cont'ed)

$$u(x) = \frac{\exp(bx/\varepsilon) - 1}{\exp(b/\varepsilon) - 1}$$







If 
$$b/\varepsilon \ll 1$$
 then  $u(x) \simeq x$ 

If 
$$b/\varepsilon \gg 1$$
 then  $u(x) \simeq \exp(-b(1-x)/\varepsilon)$ 

In the second case, boundary layer of size  $\mathcal{O}(\varepsilon/b)$ 

### Convection diffusion equation (cont'ed)

Approximation by finite elements

$$a(u,v) = \int_0^1 \left(\varepsilon u'(x)v'(x) + bu'(x)v(x)\right) dx$$

After some computations... stiffness matrix is (uniform mesh):

$$\left(\frac{b}{2} - \frac{\varepsilon}{h}\right) u_{i+1} + \frac{2\varepsilon}{h} u_i + \left(-\frac{b}{2} - \frac{\varepsilon}{h}\right) u_{i-1}$$

Local Péclet number is  $\mathbb{P}(h) = |b|h/(2\varepsilon)$ , so that our system has the structure

$$(\mathbb{P}(h) - 1)u_{i+1} + 2u_i - (\mathbb{P}(h) + 1)u_{i-1} = 0$$

 $\leftarrow$   $\rightarrow$   $\dot{}$ 

### Convection diffusion equation (cont'ed)

$$(\mathbb{P}(h) - 1)u_{i+1} + 2u_i - (\mathbb{P}(h) + 1)u_{i-1} = 0$$

#### General solution

$$u_i = \frac{1 - \left(\frac{1 + \mathbb{P}(h)}{1 - \mathbb{P}(h)}\right)^i}{1 - \left(\frac{1 + \mathbb{P}(h)}{1 - \mathbb{P}(h)}\right)^N} \quad i = 1, \dots, N$$

If  $\mathbb{P}(h) > 1$  solution oscillates!

#### Stabilization techiniques

- Upwind (finite differences)
- Artificial viscosity, streamline diffusion (loosing consistency)
- Petrov-Galerkin, SUPG (strongly consistent)

#### **Hyperbolic equations**

Let's consider the model problem (one dimensional convection equation)

$$\begin{cases} \frac{\partial u}{\partial t} + a \frac{\partial u}{\partial x} = 0, & t > 0, \ x \in \mathbb{R} \\ u(x,0) = u_0(x), & x \in \mathbb{R} \end{cases}$$

Solution is a traveling wave  $u(x,t) = u_0(x-at)$ .

We consider a finite difference approximation.

### Hyperbolic equations (cont'ed)

$$u_j^n \simeq u(x_j, t_n)$$

$$\frac{\partial u}{\partial t} + a \frac{\partial u}{\partial x} = 0$$

$$u_j^{n+1} = u_j^n - \frac{\Delta t}{\Delta x} (h_{j+1/2}^n - h_{j-1/2}^n)$$

where  $h_{j+1/2} = h(u_j, u_{j+1})$  is a numerical flux

Indeed,

$$\frac{\partial}{\partial t}U_j = -\left((au)(x_{j+1/2}) - (au)(x_{j-1/2})\right) \quad \text{with } U_j = \int_{x_{j-1/2}}^{x_{j+1/2}} u, \, dx$$

### Hyperbolic equations (cont'ed)

Courant–Friedrichs–Lewy (CFL) condition

$$\left| a \frac{\Delta t}{\Delta x} \right| \le 1$$

Very clear geometrical interpretation (see also multidimensional extension and generalization to systems)

Remark: implicit schemes (in time) don't have restrictions, but add artificial diffusion

# **End of part III**